RF 128.1291USN 19-56p-06

In the claims:

Please amend the claims as shown below:

- 1. (Currently amended) A method for the dilution of dewatered and compressed cellulose pulp that has been consolidated into large pieces, where the dewatered cellulose pulp maintains a first consistency greater than 20%, preferably greater than 25%, and even more preferably greater than 30%, whereby comprising:
 - fragmenting the cellulose pulp is fragmented into a finely divided pulp after or in association with dewatering, character rised in
- granulating that the cellulose pulp is granulated through
 fragmentation to a particle size with a normal distribution
 with a maximum size that is less than 40 mm, preferably less
 than 30 mm, and even more preferably less than 20 mm, and
 that during fragmentation maintains
- while fragmenting, maintaining a consistency of the cellulose pulp that is essentially equivalent to the first consistency, feeding that the cellulose pulp that has been finely divided through the fragmentation is fed out into a freely falling flow,
- adding that dilution fluid is added under pressure towards

 the freely falling fragmented pulp through a number of fluid jets (62) arranged in association with the flow of the freely falling fragmented pulp,
 - that the amount of dilution fluid added through the said fluid jets 462) establishes establishing a second consistency
- of the cellulose pulp in the a medium-consistency range 8-16%,
 - feeding that the cellulose pulp at this medium consistency 8-

RF 128.1261USN 19-Sep-06

5

10

15

- that the a dilution of the freely falling pulp down to a medium consistency of 8-16% before it the freely falling pulp is fed enwards enwardly to subsequent treatment stages takes taking place essentially exclusively under the an influence of hydrodynamic effect from the addition of the dilution fluid through the said fluid jets, and where no mechanical agitation takes taking place between the fragmentation of the cellulose pulp and the an underlying surface (Liquev) of the cellulose pulp that has been diluted by the dilution fluid that has been established.
- 2. (Currently amended) The method according to claim 1, c h are cterised in that wherein the fluid jets are arranged around the flow of fragmented pulp formed in the free fall, and are directed principally radially inwards towards the flow.
- 4. (Currently amended) The method according to either claim

 1 or claim 2, c h a r a c t e r i s e d i n that claim 1

 wherein the dilution fluid added is added to a degree of more than 50%, preferably more than 75-90%, through the said fluid jets (62).
- 5. (Currently amended) The method according to any one of claims 1-3, c.h a r a c t e r i s e d i n that claim 1 wherein the addition of dilution fluid from the relevant fluid jets (62) takes place in the a form of pressurized

10

- 6 -

RF 128.1281USN 19-Sep-06

pressurised fluid jets that are directed obliquely downwards downwardly in the a fall direction of fall of the cellulose pulp.

- (Currently amended) The method according to claim 4, c h 5 6. a racterised in that wherein the fluid jets are directed at an angle of 45° ± 15° relative to the a vertical direction and the a fall direction of fall of the granulate.
 - 7. (Currently amended) A device for the dilution of dewatered cellulose pulp, comprising:

shredder screw means for fragmenting pulp to a particle size in an interval of 5-40 millimeters, the shredder screw means

- having an outlet defined therein, the shredder screw means 15 containing the fragmented pulp,
 - a vertical standpipe connected to the outlet of the shredder screw means, the standpipe carrying a flow of the fragmented pulp flowing under free fall, the standpipe having a
- 20 distribution chamber defined therein at an upper end of the stand pipe, the distribution chamber arranged concentrically around the standpipe,
 - at least four nozzles arranged around a circumference of the distribution chamber, the nozzles being oriented inwardly
- 25 towards a center of the flow to add a dilution fluid under pressure into the stand pipe, the nozzles being disposed above a liquid level of diluted pulp established in the standpipe, a feed arrangement disposed at a bottom of the standpipe for

RF 128,1281USM 19-Sep-06

5

10

15

feeding the pulp to subsequent treatment stages, a pump disposed at the bottom of the standpipe and in operative engagement with the feed arrangement, and the standpipe having no mechanical agitator disposed above the liquid level. dewatoring equipment (7,80) to which pulp at an initial consistency in the range 4-12% has been fed and in which the cellulose pulp after dewatering maintains a consistency greater than 20%, preferably greater than 25%, and even more preferably greater than 30%, whereby the cellulose-pulp is fed to fragmentation equipment (8, 8b) to be fragmented into a finely-divided pulp, characterised in that the cellulose pulp is granulated through fragmentation in the fragmentation equipment (8, 8b) into a particle size with a normal distribution with a maximum size that is less than 40 mm, preferably-less than 30 mm, and even more preferably less than 20 mm, that the pulp that has been finely divided is fed from the

vertical stand pipe (22/40'), under free fall,

that a number of nozzles (62) are arranged around the

circumference of the stand pipe (22), from which nozzles

dilution fluid (LiqDIL) is added under pressure into the

stand pipe and above a level (LiqLEV) of diluted cellulose

pulp established in the stand pipe,

outlet of the fragmentation equipment into an essentially

where the amount of added dilution fluid (LiqDIL) establishes

RF 128.1281USN 19-Sep-06

5

10

15

a consistency of the cellulose pulp in the range of medium consistency 8-16% and that this added amount, to more 50%, preferably to more than 75-90%, is added through the said nozzles (62) arranged above a level (LiqLEV) established in the stand-pipe,

that the cellulose pulp at this medium consistency is fed enwards to subsequent treatment stages by a feed arrangement (41).

that the dilution of the pulp to a medium consistency of 8
16% in the stand pipe takes place exclusively under the
influence of hydrodynamic effect from the addition of
dilution fluid through the said nozzles and without the use
of a mechanical agitator above the level (LiqLEV) of fluid
established in the stand pipe (22/40)

- 8. (Currently amended) The device according to claim 7 c h a r a c t e r i s e d i n that wherein the device has the cellulose pulp at this medium consistency is fed onwards to subsequent treatment stages for the cellulose pulp with a the pump (41) connected to the stand pipe (32/40°) at its a lower part thereof close to the bottom of the stand pipe, under the liquid level (LiqLEV) of fluid established.
- 9. (Currently amended) The device according to claim 7 c h a r a c t e r i s e d in that wherein the nozzles at least four nozzles are arranged around the a periphery of the stand pipe, where the a distance between neighbouring nozzles is less than 50-300 mm (22/40-).

RF 128.1281USN 19-5ep-06

- 10. (Currently amended) The device according to claim 9 c h a r a c t e r i s c d in that wherein each nozzle is directed in towards the sentre of the stand pipe and obliquely downwards at an angle relative to the vertical and the a direction of free fall of the fragmented pulp granulate of 45 ±15°.
- 11. (Currently amended) The device according to claim 10 c

 haracterised in that wherein all nozzles are connected to a common distribution chamber (60) for dilution fluid, which the chamber is pressurised pressurized through a pressure-raising device (61).
- 12. (New) The device according to claim 7 wherein the nozzles are oriented obliquely downwardly.

15

5